

API Ballot Summary Sheet

11/4/2005

Ballot: 60-05: 650-595, Annular Plate Thickness

AMS ID: 741

Start Date: 8/29/05

Closing Date: 10/20/05

Associate: Gordon Robertson

Coordinator: Gordon Robertson

Proposal:

Vote Results

<u>Voter</u>	<u>Company</u>	<u>Comments</u>	<u>Vote Results</u>			
			<u>Affirmative</u>	<u>Negative</u>	<u>Abstain</u>	<u>Did Not Vote</u>
134629	Nelson Acosta	HMT Inspection	Yes	X		
131617	Joel Andreani	Equity Engineering Group, Inc., The	No	X		
38921	Robert Annett	Alyeska Pipeline	No	X		
73074	Ronald Bailey	American Tank & Vessel, Inc.	No	X		
136219	Mark Baker	Baker Consulting Group, Inc.	No	X		
142888	Chris Bashor	Minnesota Pollution Control Agency	No			X
134681	Ernie Blanchard	MOSAIC	No	X		
109375	Jerry Boldra	SBC Global	Yes	X		
22200	Dan Boley	DJA Inspection Services	No	X		
134782	Steve Caruthers	Tank Consultants, Inc.	No	X		
154212	Gary Cavey	Conservatek Industries, Inc.	No	X		
7127	Earl Crochet	Kinder Morgan	No	X		
150217	Jody Day	Lide Industries, Inc.	No			X
142685	Domingo de Para	ExxonMobil	No			X
133403	Jeffrey DeArmond	BP p.l.c. Whiting Refinery	No	X		
146748	Terry Delong	Terasen Pipelines (USA) Inc.	No	X		
135965	Kenneth Erdmann	Matrix Service Company	No	X		
105011	David Flight	Dow Chemical Company	No			X
134870	Laurence Foster	Marathon Ashland Petroleum LLC	No	X		
134880	John Fumbanks	Pond and Company Inc.	No			X
115033	Alan Geis	Colonial Pipeline Company	No	X		
83689	Ty Hagen	Hagen Engineering International, Inc.	No	X		
136619	Robert Hendrix	Eastman Chemical Co	Yes	X		
70596	Marty Herlevic	James Machine Works, Inc.	No	X		
93133	Randy Kissell	TGB Partnership	Yes	X		
81918	Manfred Lengsfeld		No		X	
135014	John Lieb	Tank Industry Consultants, Inc.	Yes	X		

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136274	Thomas Lorentz	AEC Engineering, Inc.	No	X	
135072	Francis Maitland	Quense LLC	No		X
113545	James McBride	Petrex, Inc.	No	X	
139045	Craig Meier	ConocoPhillips	No		X
137255	Carl Mikkola	Enbridge Energy Partners, L.P.	No	X	
131185	Douglas Miller	Chicago Bridge & Iron Company(CB&I)	No	X	
69609	Bhana Mistry	TIW Steel Platework	No	X	
83736	John Mooney		No	X	
92212	George Morovich	TEMCOR	No	X	
136286	Philip Myers	Chevron Corporation	No	X	
132210	David Nasab	Kellogg Brown & Root	No	X	
82544	John Oleyar	HMT, Inc.	No	X	
5193	Richard Pinegar	Cargill Inc.	No		X
102412	Roy Ralph	Petro-Canada	No		X
135169	Michael Richardson	International Paper	Yes	X	
73744	Bruce Roberts		No	X	
101360	Marilyn Shores	Sunoco Logistics	No	X	
126019	Larry Speaks	Mass Technology Corporation	No	X	
134314	Tearle Taylor	Flint Hills Resources	No	X	
134325	Donald Thain	Shell Global Solutions (US) Inc.	Yes	X	
145034	Leith Watkins	Explorer Pipeline Company	No		X
145896	Alan Watson	A.R. Watson, USA	No	X	
132209	Richard Whipple	Fluor, Inc.	No	X	

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	<u>Affirmative</u>	<u>Negative</u>	<u>Abstain</u>	<u>Did Not Vote</u>
Balloting Totals:	39	0	1	10

Total Responses:	40	
Total Ballots:	50	
Response Rate :	78%	Must be > 50%
Approval Rate:	100%	Must be > 67%
Consensus:	YES	

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134629 Nelson Acosta

HMT Inspection

Specification Section

Type

Comment

Suggested Change

3.5.3, footnote b and term definition

Editorial

Remove the second "the" in the first sentence as unnecessary.

Footnote b: Add a period to end the first sentence after "test stress)".

In the second sentence, reference to "a" should read "per footnote a" and later in the same sentence, a comma should be added between "thickness" and "then".

In the definition of terms (if these definitions are to be added to the final text), correct the spelling of "fully" in the definition of "tr".

3.5.3 The thickness of annular bottom plates shall not be less....

footnote b: The stress to be used is the maximum stress in the first shell course (greater of product or hydrostatic test stress). The stress may be determined by using the thickness per footnote a divided by the required thickness, then multiplied by the applicable allowable stress:

tr = API recommended annular thickness from Table 3-1 if shell fully stressed at hydro

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109375 Jerry Boldra

SBC Global

<u>Specification Section</u>	<u>Type</u>	<u>Comment</u>	<u>Suggested Change</u>
Proposed Paragraph 3.5.3 . . . last sentence	Editorial	The last sentence leaves the reader hanging . . . because the final part of the sentence has been omitted. See below:	Choose the correct final phrase . . . and add it to the end of the last sentence, either: 1) . . . TO DETERMINE THE ANNULAR PLATE THICKNESS. 2) . . . TO DETERMINE THE THICKNESS OF THE FIRST SHELL COURSE. 3) . . . TO DETERMINE THE THICKNESSES OF THE ANNULAR PLATE AND THE FIRST SHELL COURSE.

136619 Robert Hendrix

Eastman Chemical Co

<u>Specification Section</u>	<u>Type</u>	<u>Comment</u>	<u>Suggested Change</u>
Foot Note b, Table 3-1	Editorial	Symbols td, Sd, tt, and St are not defined.	Add informative comment, "where td, Sd, tt, and St are as defined in 3.6.3.2"
Explanation of Item	Editorial	I can't seem to find the attachment to which you refer. Is it on some earlier submittal?	

93133 Randy Kissell

TGB Partnership

<u>Specification Section</u>	<u>Type</u>	<u>Comment</u>	<u>Suggested Change</u>
3.5.3	Editorial	Change "M" to "m" (abbreviation for meters) and delete "or =".	
Table 3-1	Technical	Footnote b: shouldn't it instead be: Product Stress = (td / supplied t exclusive of CA) (Sd) Hydrostatic Test Stress = (tt / supplied t) (St)	

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135014 John Lieb

Tank Industry Consultants, Inc.

Specification Section	Type	Comment	Suggested Change
Table 3-1	Technical	I think we should also delete the word "nominal" frm the first column headings in Table 3-1. This has been a source of confusion in the past.	Delete "nominal" from 1st column heading for SI Units and US Customary portions of Table 3-1.
Proposed footnote b	Technical	We should retain the reference to 3.6.3.2 in the new version of footnote b. Otherwise, the use of td may be unclear.	Insert "(See 3.6.3.2)" after "Product Stress = (supplied t exclusive of CA / td) (Sd)"

135169 Michael Richardson

International Paper

Specification Section	Type	Comment	Suggested Change
General	Technical	It is not uncommon in the Pulp & Paper Industry to store products with specific gravities in the range of 1.5 to 1.9. Have you considered your analysis at these higher specific gravities?	

134325 Donald Thain

Shell Global Solutions (US) Inc.

Specification Section	Type	Comment	Suggested Change
Table 3-1, footnote a	Technical	If the term "nominal" thickness is to be revised, then the first column in the table needs to reflect the modified terminology.	
Table 3-1, footnote b & c	Editorial	Delete current footnote c. Change table to only reference footnote b.	
Table 3-1, footnote b & c	Technical	Td, Tt, Sd, St are new to this table and not defined in this section	

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