

**Linings of Aboveground Petroleum Storage Tank  
Bottoms**

**API Recommended Practice 652**

~~Third Edition, October 2005~~

Fourth Edition, November 2012

Committee Draft

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# Linings of Aboveground Storage Tank Bottoms

## 1 Scope

This recommended practice provides guidance on achieving effective corrosion control in aboveground storage tanks by application of tank bottom linings. It contains information pertinent to the selection of lining materials, surface preparation, lining application, cure, and inspection of tank bottom linings for existing and new storage tanks. In many cases, tank bottom linings have proven to be an effective method of preventing internal corrosion of steel tank bottoms.

The intent of this recommended practice is to provide information and guidance specific to aboveground steel storage tanks in hydrocarbon service. Certain practices recommended herein may also be applicable to tanks in other services. This recommended practice is intended to serve only as a guide. Detailed tank bottom lining specifications are not included.

This recommended practice does not designate specific tank bottom linings for every situation because of the wide variety of service environments.

NACE No.10/SSPC-PA 6 and NACE No. 11/SSPC-PA 8 are industry consensus standards for installation of linings on tank floors and vessels. They are written in compulsory language and contain specific criteria intended for use by persons who provide written specifications for tank and vessel linings. These documents should be given consideration when designing and installing a lining system for steel bottom tanks.

## 2 References

### 2.1 Codes, Standards, and Specifications

Unless otherwise specified, the most recent edition or revision of the following standards, codes, or specifications shall, to the extent specified herein, form a part of this recommended practice.

#### API

- RP 575 Inspection of Atmospheric and Low-Pressure Storage Tanks
- ~~STD~~ 620 Design and Construction of Large, Welded, Low-Pressure Storage Tanks
- ~~STD~~ 650 Welded Steel Tanks for Oil Storage
- RP 651 Cathodic Protection of Aboveground Petroleum Storage Tanks
- ~~STD~~ 653 Tank Inspection, Repair, Alteration, and Reconstruction
- ~~STD~~ 2015 Requirements for Safe Entry and Cleaning of Petroleum Storage Tanks
- RP 2016 Guidelines and Procedures for Entering and Cleaning Petroleum Storage Tanks

#### ASTM

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D 2583 Standard Test Method for Indentation Hardness of Rigid Plastics by Means of a Barcol Impressor ~~—Impressor~~

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D 4414 Standard Practice for Measurement of Wet Film Thickness by Notch Gauges

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D 4417 Standard Test Methods for Field Measurement of Surface Profile of Blast Cleaned Steel

D 4940 Standard Test Method for Conductimetric Analysis of Water Soluble Ionic Contaminants of Blasting Abrasives

D 5402 Standard Practice for Assessing the Solvent Resistance of Organic Coatings Using Solvent Rubs

E 96 Standard Test Methods for Water Vapor Transmission of Materials

G 9 Standard Test Method for Water Penetration into Pipeline Coating

#### **DSTAN**

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Defense Standard

80-97 Paint System, Medium Build for the Interior of Bulk Fuel Tanks and Fittings

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#### **ISO Standard**

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8502-3 Preparation of steel substrates before application of paint and related products – Tests for the assessment of surface cleanliness.

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#### **Military Standards**

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MIL-PRF

UFGS 09 97 13.15 Epoxy/Fluoropolyurethane Interior Coating of Welded Steel Petroleum Fuel Tanks

4556 Coating Kit, Epoxy for Inter or Steel Fuel Tanks

~~N23236 Coating Systems for Ship~~

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#### **NACE**

37519 Corrosion Data Survey—Metals Section

TM0174 Laboratory Methods for the Evaluation of Protective Coatings and Lining Materials on Metallic Substrates in Immersion Service

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- RP0188 Discontinuity (Holiday) Testing of New Protective Coatings on Conductive Substrates
- RP0178 Fabrication Details, Surface Finish Requirements, and Proper Design Considerations for Tanks and Vessels to be Lined for Immersion Service
- RP0287 Field Measurement of Surface Profile of Abrasive Blast Cleaned Steel Surfaces Using a Replica Tape

**NACE/SSPC**

NACE No. 1/ White Metal Blast Cleaning

SSPC-SP 5

NACE No. 2/ Near-White Metal Blast Cleaning

SSPC-SP 10

NACE No. 5/ Joint Surface Preparation Standard:

SSPC-SP 12 Surface Preparation and Cleaning of Metals by Waterjetting Prior to Recoating

NACE No. 10/ Fiberglass-Reinforced Plastic (FRP)

SSPC-PA 6 Linings Applied to Bottoms of Carbon Steel Aboveground Storage Tanks

NACE No. 11/ Thin-Film Organic Linings Applied in New

SSPC-PA 8 Carbon Steel Process Vessels

NACE 6A192/ Dehumidification and Temperature

SSPC-TR 3 Control During Surface Preparation, Application, and Curing for Coatings/Linings of Steel Tanks, Vessels, and Other Enclosed Spaces

SSPC SP-1 Solvent Cleaning

SSPC SP-11 Power Tool Cleaning- to Bare Metal

~~SSPC SP-1 Solvent Cleaning~~

**OSHA**

29 CFR

1910.1000 Air Contaminants

1910.1200 Hazard Communication

1910.94 Ventilation

1910.132 Personal Protective Equipment, General Requirements

1910.134 Respiratory Protection

1910.146 Permit-Required Confined Spaces

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~~1926.62~~ ~~Lead~~

~~1910.134~~ ~~Respiratory Protection~~

1910.147 The Control of Hazardous Energy (Lockout/Tagout)

1910.94 Ventilation

~~1910.1000~~ ~~Air Contaminants~~

~~1910.1200~~ ~~Hazard Communication~~

1926.354 Welding, Cutting, and Heating in way of Preservative Coatings

1926.62 Lead

Publ. 2254 Training Requirements in OSHA Standards and Training Guidelines

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## **SSPC**

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PA 1 Shop, Field, and Maintenance Painting

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PA 2 Measurement of Dry Paint Thickness with Magnetic Gages

PA 3 A Guide to Safety in Paint Application

~~SP 1~~ ~~Solvent Cleaning~~

~~SP 11~~ ~~Power Tool Cleaning to Bare Metal~~

~~TU 4~~~~Guide 15~~ ~~Field Methods for Retrieval and Analysis of Soluble Salts on Substrates~~~~Field Methods for Retrieval and Analysis of Soluble Salts on Steel and Other Nonporous Substrates~~

VIS 1 Guide and Reference Photographs for Steel Surfaces Prepared by Dry Abrasive Blast Cleaning

## 2.2 Other References

Although not cited in the text, these publications may be of interest or contain related material.

## **API**

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RP 2009 Safe Welding, Cutting and Hot Work Practices in the Petroleum & Petrochemical Industries

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Publ. 2207 Preparing Tank Bottoms for Hot Work ~~Work~~

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**ACGIH**

Threshold Limit Values (TLVs®) and Biological Exposure Indices (BEIs®)

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**NACE**

Handbook 1 Forms of Corrosion Recognition and Prevention, Vol. 1 & 2

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**OSHA**

**29 CFR**

- 1910.134 Respiratory Protection
- 1910.147 The Control of Hazardous Energy (Lockout/Tagout)
- 1910.1000 Air Contaminants
- 1910.1200 Hazard Communication
- 1926.354 Welding, Cutting, and Heating in way of Preservative Coatings

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**SSPC**

- AB 1 Mineral and Slag Abrasives
- AB 2 Specification for Cleanliness of Recycled Ferrous Metallic Abrasives
- AB 3 Newly Manufactured or Re-manufactured Steel Abrasives

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**3 Definitions**

3.1 aboveground storage tank: A stationary container, usually cylindrical in shape, consisting of a metallic roof, shell, bottom, and support structure where more than 90% of the tank volume is above surface grade.

~~3.2 adduct: A curing agent, generally an amine that has been combined with a portion of the resin, usually an epoxy.~~

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~~3.3 amine: An organic compound having amino functional groups, which provide chemical reactivity and ability as a curative for epoxy and other resins.~~

3.24 anchor pattern: Surface contour or roughness of a blast cleaned or substrate surface, when viewed from the edge. Also called profile, surface profile or roughness. ~~Surface contour of a blast cleaned or substrate surface, when viewed from the edge (cross-section of the surface). See profile.~~

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3.35 anode: The electrode of an electrolytic cell at which oxidation is the principal reaction. (Electrons flow away from the anode in the external circuit. It is usually the electrode where corrosion occurs and metal ions enter solution.)

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The electrode of an electrochemical cell at which oxidation (corrosion) occurs. Electrons flow away from the anode in the external circuit. Corrosion usually occurs and metal ions enter the solution at the anode.

3.6 aromatics: A type of solvent based on Benzene ring molecules (e.g. Benzene, Toluene and Xylene). Strong hydrocarbon solvents whose chemical structure has one or more unsaturated ring structures. Benzene, toluene, and xylene are common examples of aromatic solvents.

3.7 Bisphenol A polyester: A polyester whose chemical structure incorporates Bisphenol A into the resin molecule in place of some or all of the glycol. The solid resin is generally provided as a solution in styrene, which acts as a solvent and as a cross-linking agent for the resin.

3.4 caulk: Products used to fair or smooth surfaces as well as seal seams and rivets in lining applications.

Caulk: Products used to fair or smooth surfaces as well as seal seams and rivets in lining applications. Bob do find or develop a definition

3.58 cathode: The electrode of an electrolytic cell at which reduction is the principal reaction. Electrons flow toward the cathode in the external circuit. The electrode of an electrochemical cell at which a reduction is the principle reaction. Electrons flow toward the cathode in the metal component.

3.69 cathodic protection: A corrosion control system in which the metal to be protected is made to serve as a cathode, either by the deliberate establishment of a galvanic cell or by impressed current. (see anode and cathode). A technique to reduce corrosion of a metal surface by making that surface the cathode of an electrochemical cell.

~~3.70 coal tar: A black hydrocarbon residue remaining after coal is distilled. Obsolete~~

~~3.74 coal tar epoxy: A combination of epoxy, curing agent, and tar products which give a very water resistant film. Obsolete~~

3.82 coating: A paint or other finish used to create a protective or decorative layer. See definition for lining. Various protective materials applied to tank surfaces, including paint, protective metals (e.g. galvanizing or cadmium plating), and adhered plastic or polyolefin materials. For coatings in immersion service (i.e., inside a tank) see the definition of "lining". NACE definition: A paint, varnish, lacquer or other finish used to create a protective and/or decorative layer. See definition for lining. liquid, liquefiable or plastic composition that has been converted to a solid protective or functional adherent film after application as a thin layer.

3.913 concentration cell: An electrolytic cell, the emf of which is caused by a difference in concentration of some component in the electrolyte. (This difference leads to the formation of discrete cathode and anode regions).

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3.143 copolymer: A large molecule whose chemical structure consists of at least two different monomers.

3.10154 corrosion: The chemical or electrochemical reaction between a material, usually a metal, and its environment that produces a deterioration of the material and its properties. The deterioration of a material, usually a metal, because of a reaction with its environment.

3.1165 cure, curing: The process whereby a liquid coating becomes a hard film. Curing is complete when the lining is ready to accept immersion in the designated service. Methods of testing cure include solvent rub and hardness testing. Curing is complete when the lining is ready to accept immersion in the designated or designed service. See solvent rub test or hardness test or glossometer here also. The setting up or hardening, generally due to a polymerization reaction between two or more chemicals (resin and curative).

3.1276 dew point: Temperature at which moisture will condense from humid vapors into a liquid state. The temperature at which moisture condenses from the atmosphere.

3.1387 differential aeration cell (oxygen concentration cell): A concentration cell caused by differences in oxygen concentration along the surface of a metal in an electrolyte. (See concentration cell). An electrochemical cell, the electromotive force of which is due to a difference in air (oxygen) concentration at one electrode as compared with that at another electrode of the same material.

3.1498 electrochemical cell: An electrochemical system consisting of an anode and a cathode in metallic contact and immersed in an electrolyte. (The anode and cathode may be different metals or dissimilar areas on the same metal surface). A system consisting of an anode and a cathode immersed in an electrolyte so as to create an electrical circuit. The anode and the cathode may be different metals or dissimilar areas on the same metal surface.

3.152019 electrolyte: A nonmetallic substance that carries an electric current, or a substance which, when dissolved in water, separates into ions which can carry an electric current. A chemical substance containing ions that migrate in an electric field.

3.16210 epoxy: Extremely tough and durable synthetic coating resins that are highly resistant to chemicals, abrasion, moisture and, in some cases, alcohols. The technical definition is a group having the oxirane structure, if anyone really cares. A better definition would be just to say: Extremely tough and durable synthetic coatings that are highly resistant to chemicals, abrasion, moisture. Not all epoxies are suitable for alcohol. Resin containing epoxide (oxirane) functional groups that allow for curing by polymerization with a variety of curatives. Epoxy resins are usually made from Bisphenol A and/or Bisphenol F and epichlorohydrin.

3.1722+ forced-curing: Acceleration of curing by increasing the temperature above ambient, accompanied by forced air circulation.

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3.18232 holiday: A discontinuity in a protective coating that exposes unprotected surface to the environment. Application defects whereby small areas are left uncoated.

3.19 lining: A liq. ~~Application defects whereby small areas are left uncoated. (SSPC)~~

~~3.25.1 lining: A material applied to the internal surfaces of a tank to serve as a barrier to corrosion and/or product contamination. The term coating is also used for the purposes of this document. A. What about 100% solids epoxy? liquid paint that develops strong adhesion to the substrate and is designed for immersion service or vapor-space service.~~

~~Note: This definition is not really necessary, polyesters are functionally obsolete.~~

~~3.25.4 lining: A material applied to the internal surfaces of a tank to serve as a barrier to corrosion and/or product contamination. The term coating is also used for the purposes of this document. A. What about 100% solids epoxy? liquid paint that develops strong adhesion to the substrate and is designed for immersion service or vapor-space service.~~

A coating applied to the interior surfaces of a vessel that is designed for immersion service or vapor-space service for a specified stored product. A lining can be reinforced or un-reinforced.

(proposed API 650 definition)

3.2065 mil: One one-thousandth of an inch (0.001 in.). One mil = 25.4 μm; it is common practice to use 1 mil = 25 μm.

3.2176 mill scale: The heavy oxide layer formed during hot fabrication or heat treatment of metals, typically a black-blue colored smooth layer found on the surface. An oxide layer formed on steel during hot forming operations, typically "gun metal" blue in color.

3.228 phenolic: A resin of the phenol formaldehyde type. 7 phenolic: A resin of the phenol formaldehyde type. The distinctions between phenolics and novolacs are not the clear anymore. Much has to do with marketing Phenolic and novolac epoxies tend to be more chemically resistant.

3.298 polyamide: A resin whose chemical structure contains adjacent carbonyl and amino functional groups that is often used as a curative for epoxy resins. Commercially available polyamides are reaction products of dimerized and trimerized fatty acids with ammonia or polyamines.

3.3029 polyamidoamine: A resin whose chemical structure contains adjacent carbonyl and amino functional groups that is often used as a curative for epoxy resins. Commercially available polyamidoamines are reaction products of monofunctional fatty acids and amines.

Note: These three definitions really add no value to the user.

Need a definition for primer that is specific to this document — Bob

P3.23 primer: First complete coat of applied to the prepared surface. Holding primers are often used in tank linings when operational issues required daily coating of the blasted surface.

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3.2431 profile: See anchor pattern. Anchor pattern on a surface produced by abrasive blasting or acid treatment.

3.320 resin: Synthetic organic ion exchange material, such as the high capacity cation exchange resin widely used in water softeners. A natural or synthetic substance that may be used as a binder in coatings.

Note: Definition not needed.

3.2533+ thick-film lining: A lining with a dry film thickness of 20 mils (5000.51 μm) or more.

3.342 thick film reinforced lining: See 6.3 for interpretation.

Note: Don't include here if not defining the term.

3.26353 thin-film lining: A lining with a dry film thickness less than 20 mils (5000.51 μm).

See 6.3 for further clarifications.

3.27364 vinyl ester: A polyester that usually contains Bisphenol A in the resin backbone and two vinyl groups for polymerization reactivity. The solid resin is generally provided as a solution in styrene, which acts as a solvent and as a cross linking agent for the resin.

A resin that very chemically resistant and is frequently used in flake coatings as well as in the fiberglass reinforced thick film systems. This product contains styrene, which is on the HAPS list and is a carcinogen.

3.28375 vinyl group: A functional group on a resin molecule that consists of a carbon-to-carbon double bond at the end of the molecule.

3.386 volatile organic compound (VOC): Compounds that have a high vapor pressure [greater than 0.27 kPa (2 mm of mercury) at 25°C] and low water solubility, excluding methane. VOCs typically are industrial solvents, fuel oxygenates, or components of petroleum fuels. VOC content in coatings is highly regulated. Specifiers should be aware of the jurisdiction and regulations in the geography where the coating is to be applied prior to specifying a coating product.

## 4 Corrosion Mechanisms

### 4.1 General

Corrosion rates of carbon steel in various hydrocarbons have been determined and are given in many reference texts such as "NACE Corrosion Data Survey-Metals Section." These rates apply only if there are no accelerating mechanisms. For example, corrosion would not be expected in ambient temperature crude oil or product service with no water present; however, corrosion may occur when a layer of water settles to the bottom of a crude oil, intermediate product, or finished product storage tank. This water, which may enter the tank with the product, through the seals, or during "breathing" of the tank, often contains corrosive compounds. For example, crude oil may contain salt water and sediment that settles out on the bottoms of storage tanks. Chlorides and other soluble salts

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contained in the water may provide a strong electrolyte that can promote corrosion. The common mechanisms of internal tank bottom corrosion include:

- a. Chemical corrosion.
- b. Concentration cell corrosion.
- c. Galvanic cell corrosion.
- d. Corrosion caused by sulfate-reducing bacteria.
- e. Erosion-corrosion.
- f. Fretting-related corrosion.

These mechanisms are discussed in detail in the following sections.

#### 4.2 Chemical Corrosion

Chemical corrosion may occur in environmental and product cleanup tanks as well as in chemical storage facilities. For example, a wastewater treatment tank operates by adding heat and/or concentrated sulfuric acid to the water to break the emulsion of oil and water. The acid, unless added properly, immediately becomes diluted and hence much more corrosive, especially in the area of the acid inlet piping. Chemical attack is also prevalent in corrosive services such as caustic, sulfuric acid, ballast water, and water neutralization services. Proper coating selection is crucial when considering this type of service.

#### 4.3 Concentration Cell Corrosion

Concentration cell corrosion may occur when a surface deposit, mill scale, or crevice creates a localized area of lower oxygen concentration. The area under a surface deposit may be penetrated by a thin layer of electrolyte, which soon becomes depleted of oxygen. The difference in oxygen concentration between the inaccessible area and the bulk electrolyte creates a galvanic cell, with the contact area of the surface deposit being anodic to the surrounding tank plate. Concentration cell corrosion will cause pitting and may result in significant localized metal loss. Pitting of a bare steel tank bottom may occur at a rate as high as 80 mils (2.0 mm) per year.

#### 4.4 Galvanic Cell Corrosion

Hot-rolled carbon steel, typically used for the construction of petroleum storage tanks, is covered with a thin layer of oxide called mill scale, which is cathodic to the base steel. In the presence of a corrodent (such as dissolved oxygen) and an electrolyte, a galvanic corrosion couple forms at breaks in the mill scale. Accelerated pitting corrosion of the steel at breaks in the mill scale can result. Mill scale may be removed from both sides of the tank bottom plate by abrasive blast cleaning or by pickling, but removal of mill scale from the underside of the steel bottom is not commonly done. Removal of mill scale from the underside of new steel bottoms may be considered in an effort to promote a more uniform corrosion and minimize accelerated pitting corrosion that may occur.

In some cases, welding can produce large differences in the microstructure of a steel bottom plate resulting in a built-in galvanic couple. In the presence of a corrodent and an

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electrolyte, preferential corrosion can occur at the heat-affected zones (HAZ) of the base metal near the welds. This type of corrosion can cause significant localized metal loss.

#### **4.5 Microbiologically Influenced Corrosion (MIC) Caused by Sulfate-Reducing Bacteria**

Sulfate-reducing bacteria (SRB) [e.g., Sulfate Reducing Bacteria (SRB) and Acid Producing Bacteria (APB)] are widespread in the petroleum industry. The role of bacteria SRB in corrosion is universally recognized but the mechanisms are not well understood. Generally, the effect of bacteria SRB on the corrosion of bare steel tank bottoms is negligible. In some cases, however, severe corrosion has been attributed to MICSRB. The bacteria SRB colonies form deposits on the steel that may provide an effective barrier to the diffusion of dissolved oxygen. Thus, the mere physical presence of bacterial deposits can promote aggressive pitting corrosion by the concentration cell mechanism described in 4.3.

The metabolism of bacteria SRB is important with regard to the corrosion of storage tank bottoms. Most bacteria found in the petroleum industry SRB are strict anaerobes that do not proliferate in the presence of oxygen; however, the dense bacterial colonies create a local anaerobic condition even if some oxygen is available. By creating the local anaerobic condition, the bacteria can stay alive in the presence of oxygen even though the colonies do not expand. In the case of SRB, colonies derive energy principally from the reduction of sulfates to sulfide, and this metabolic end product is corrosive to steel. Moreover, the iron sulfide corrosion product is cathodic to the base steel and may promote accelerated pitting corrosion by a galvanic mechanism as described in 4.4, if dissolved oxygen is available as a corrodent. This type of corrosion can often be found in tanks containing diesel and fuel oils.

#### **4.6 Erosion-Corrosion**

Erosion-corrosion may occur in wastewater treating or mixing tanks where soil or small abrasive aggregate is present. To a lesser extent, erosion-corrosion can also occur at tank mixers in crude oil storage tanks. A water treatment tank blends chemicals into contaminated water to break any emulsions of oil and water. Agitation may increase corrosion by delivering more corrodent, such as dissolved oxygen, from the bulk of the stored product to the surface of the tank steel. Turbulence also moves any fine aggregate that is present, creating an abrasive environment in which adherent, semi-protective corrosion products can be dislodged, exposing the underlying steel to the corrosive environment. Severe erosion conditions may scour the base metal directly. Erosion-corrosion causes highly localized metal loss in a well-defined pattern. Erosion corrosion may be found at tank inlets and outlets where product flow occurs.

#### **4.7 Fretting-Related Corrosion**

Fretting-related corrosion may occur in hydrocarbon service on the bottoms of external floating roof tanks. When the tank is emptied, the floating roof is typically supported on roof-support legs constructed of open-ended pipe. Most bottom designs require “striker plates” under each roof support leg. When the floating roof is landed, the pipe legs rest on the striker plates supporting the weight of the roof. Repeated, frequent contact between

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the striker plate and the open end of the pipe leg removes any protective layer of rust scale that may have formed on the striker plate surface. When the roof is floated again, any water on the tank bottom causes corrosion at the location on the striker plate where the coating and/or any protective rust scale has been damaged. Experience has shown that frequent roof landings over a long period of time causes corrosion severe and localized enough to corrode a hole through the striker plate and the floor plate like a cookie cutter.

## 5 Determination of the Need for Tank Bottom Lining

### 5.1 General

The bottom plates of aboveground storage tanks are susceptible to internal and external corrosion. Storage tank bottoms are generally fabricated from carbon steel plate sections that are typically 0.25 in. (6 mm) thick. Annular floor plates of storage tanks frequently have thicker plate sections ranging from 0.25 to 1.0 in. (6 to 25 mm). The bottom plate sections and the attachment fillet lap welds are intended to function as a membrane and prevent leaks. Uniform soil support beneath the bottom plate minimizes stress in the bottom plate.

The need for an internal tank bottom lining in an aboveground storage tank is generally based on several considerations:

- a. Corrosion prevention.
- b. Tank design.
- c. Tank history.
- d. Environmental considerations.
- e. Reduce time and effort for future tank cleaning.
- f. Federal, state, and local regulations.
- g. Product quality.
- h. Considerations under API 653 with respect to next inspection interval.

### 5.2 Linings for Corrosion Prevention

The proper selection, application, and maintenance of tank bottom linings can prevent internal corrosion of the steel tank bottom. Unless means of corrosion prevention are used on the soil side, perforation of the tank bottom may still occur.

The minimum thickness of the steel tank bottom should be determined according to API Std 653. An internal tank bottom lining may be deemed necessary if inspection shows that the minimum thickness of the bottom steel plate is less than 0.100 in. (2.5 mm), or if corrosion is expected to proceed so that the steel thickness may reach this minimum thickness, - generally 0.100 in (2.5 mm), prior to the next scheduled inspection.

If the minimum bottom thicknesses, at the end of the in-service period of operation, are calculated to be less than the minimum bottom renewal thicknesses given in Table 4.4 (API 653), or less than the minimum bottom renewal thicknesses providing acceptable

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risk as determined by an RBI assessment per 6.4.2.4 (API 653), the bottom shall be lined, repaired, replaced, or the interval to the next internal inspection shortened.

Taken from API 653 e4 wAdd1

When using API ~~STD~~ 653 to determine appropriate internal inspection intervals for aboveground storage tanks, the anticipated life of the lining as well as the corrosion rate anticipated in the event of premature lining failure should be considered. Note: This is why I would change the 5.2 as shown above.

### 5.3 Tank Corrosion History

The corrosion history of a particular tank should be considered when determining the need for an internal lining. The corrosion history of tanks in similar service should also be considered. The items to be considered are dictated by individual circumstances, but some of the more important considerations are as follows:

- a. Where is the corrosion occurring (product side, soil side, or both)?
- b. What is the internal and soil-side corrosion rate?
- c. Have there been significant changes in the corrosion rate?
- d. Is the corrosion uniform or localized ~~What type of corrosion is occurring?~~
- e. Has corrosion caused perforation of the steel tank bottom?
- f. What was the prior service of the tank and how corrosive was that product?

### 5.4 Tank Foundation

The foundation must be adequate to prevent excessive settlement of the tank. If uniform foundation support is not provided, flexing of the tank bottom can result as the tank is filled or emptied. Flexing occurs on all steel floors; however, excessive flexing of the steel bottom may cause an internal bottom lining to crack.

The tank pad material beneath the steel bottom has a significant effect on the potential for underside corrosion. If there is pad contamination (e.g. rock, lumps of clay, welding electrodes, paper, plastic, wood, etc.) in contact with the underside of the steel, differential aeration or other corrosion cells can form where the contaminants are in contact with the tank bottom and severe corrosion may result (see API RP 651). The use of wood under a tank floor is not recommended given that it promotes bacterial activity and will cause accelerated corrosion.

## 6 Tank Bottom Lining Selection

### 6.1 General (add to this section a statement about the use of primers concerning consideration of the surface of the steel. - Bob)

Tank bottom linings can generally be divided into two classes: thin-films [with a dry film thickness less than 20 mils (~~5000.51~~  $\mu\text{m}$ )] and thick-films [with a dry film thickness of 20 mils (~~5000.51~~  $\mu\text{m}$ ) or more]. Linings may be applied to the bottoms of storage tanks

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when they are first constructed or they may be installed after some period of service. Generally, thin-film linings may be applied to new tanks and to bottoms of storage tanks that have experienced minimal corrosion. The advantages and disadvantages of thin and thick-film tank bottom lining systems are discussed in this section.

Most tank bottom lining materials are initially selected based on chemical resistance or compatibility with the stored product. However, resistance to moisture permeation should also be a major consideration for long-term service since most storage tanks will typically have a layer of water on the floor. All lining materials absorb moisture over time and this absorption can ultimately result in its failure. The moisture vapor transmission of various lining materials can be comparatively tested using ASTM E 96, ASTM G 9, or other equivalent test methods. Because tank bottoms flex during operation, a bend test on coating candidates should be performed to ASTM standards prior to coating selection, ASTM D 522 Replace with ASTM bend test (Jerry Woodson or Eddie Borne to provide), or another appropriate standard. Note: What is an acceptable criteria, if this test is performed? This creates more questions than it answers.

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Recent advancements in technology have produced coatings with zero VOCs. These 100% solid coatings provide reduced safety concerns during the application; can be applied in a single coat and offer a reduction in the tank turnaround schedule. With exceptions, typically these coatings are classified as thick-film linings although 100% solids coatings may be applied as thin film linings where the excess thickness is not required.

## 6.2 Thin-Film Tank Bottom Linings

Thin-film tank bottom lining systems are frequently based on epoxy or epoxy-copolymer resins. ~~Table 1 lists several generic types of thin film linings and their suitability for various stored hydrocarbon and petrochemical products.~~ All linings that are employed to protect tank bottoms also must be resistant to water, since water must be present at the tank bottom for electrochemical corrosion to occur. NACE No. 11/SSPC-PA 8 should be given consideration when designing and installing a thin-film lining system for steel bottom tanks.

Table 1—Thin film Tank Bottom Lining Systems

### Lining Systems<sup>a</sup>

(resin/curative) — Typical Services — Maximum Temperature Range

°F (°C)<sup>b</sup>

Coal tar epoxy/amine — Foul water services and crude oil — 120–170 (49–77)

Epoxy phenolic/amine (i.e. novalac) — Light products, distillates, aromatics, high purity water, sour products, crude, and gasoline — 180–220 (82–104)

Epoxy/amine — Water, light products, distillates, aromatics, crude, and gasoline — 160–220 (71–104)

Epoxy/polyamide — Water, distillates, crude, and gasoline — 160–180 (71–82)

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~~Epoxy/polyamidoamine — Water, distillates, crude, and gasoline — 160-180 (71-82)~~

~~Note: This table is of little or no value to the users of this document. It is been remaining here from many years ago and is not up to date with coating technology.~~

~~Note:~~

~~a. — Generally applied over a white or near white abrasive blast cleaning in two or three coats. No primer is required. By definition the first coat is the primer. Information related to the performance limitations of specific coatings with regard to chemical immersion and elevated temperatures should be obtained from the lining manufacturer.~~

~~b. — For tanks containing a water layer on the bottom, the maximum temperature will be at the lower end of the specified range.~~

~~e. Inorganic zinc (zinc silicates) are often applied to internal tank surfaces. These coatings are typically applied at 3-5 mils DFT. These linings are not considered thin film linings for purposes of API 653 calculations.~~

~~Note: Use of these coatings needs to be addressed as they are often specified for ethanol/methanol service and biodiesel.~~

#### 6.2.1 Advantages of Thin-film Linings

Thin-film lining systems are often used for application to the topside of the bottoms of new storage tanks. New steel plates provide a smooth surface that easily can be made ready for lining application. Corrosion of bare steel tank bottoms is rarely uniform. Generally, corrosion due to immersion exposure creates a surface that is rough and pitted, and it is often difficult to completely coat and protect a corroded steel bottom with a thin-film lining system. The principal advantages of thin-film linings are as follows:

- a. Initial cost is typically less than thick-film reinforced linings.
- b. Most are easier to apply than thick-film reinforced linings.
- c. Experience has shown that when properly selected, applied, and not damaged, the life of thin-film linings can be greater than 20 years.
- d. Most thin-film epoxy linings exhibit good flexibility.
- e. Generally more accurate MFL floor scans.
- f. It is often easier to remove a thin-film lining at the end of its useful life.

~~g. Thin film linings may be all that is needed to prevent internal corrosion from occurring based on the condition of the steel substrate.~~

#### 6.2.2 Limitations of Thin-film Linings

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a. API STD ~~td-653~~, allows requires a minimum of 0.050 in. (1.3 mm) remaining bottom plate thickness at the next internal inspection, if when thick-film, reinforced linings are used. Thick-film reinforced linings may be used to extend the inspection interval depending on the particular tank inspection results and calculations.

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-In the case of thin-film linings, hHowever, for thin film linings, API STD ~~td-653~~ only allows requires the bottom plate thickness be a minimum of 0.100 in. (2.5 mm) at the end of the next service interval.

b. Thin-film linings are more susceptible to mechanical damage than thick-film linings.

c. Rough weld surfaces and weld spatter can protrude through the finished lining thickness and result in holidays, therefore, weld surfaces should be relatively smooth and weld spatter removed before a lining is applied. Alternately, caulking compatible with the lining product may be used to cover rough welds. If it is not feasible to create relatively smooth welds free from weld spatter by grinding or other processes, caulking or thick-film coatings may be considered as an alternative in order to create a film free from holidays. Optimally, requirements for weld surface quality are part of the welding specification and not part of the lining contractor's responsibility. In the case of reinforced thick film systems, caulking may be part of the requirements for proper installation. See NACE 10/SSPC-PA6 Fiberglass-Reinforced Plastic (FRP) Linings Applied to Bottoms of Carbon Steel Aboveground Storage Tanks for information on caulking.

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d. Some thin-film linings require the application of multiple coats.

e. Thin-film linings are most often solvent-borne coatings that require the evaporation of solvent from the film to achieve proper cure. If the solvent vapors are not effectively removed from the tank or vessel, because they are heavier than air, they will hover at the floor level and impede the progress of the cure. VOC regulations shall be considered when specifying thin film coatings.

f. Presence of moisture in the air during the cure can cause amine blush, which must be removed before the application of subsequent coats. Amine blush can cause issues with intercoat adhesion if not properly removed- between coats.

### **6.3 Thick-Film, Reinforced Tank Bottom Linings**

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**Thick-film, reinforced linings may be used as tank bottom linings for both new and old storage tanks. Table 2 lists generic types of resins typically used in such linings. These resins are commonly reinforced with chopped glass fibers, chopped glass mat, woven glass mat, or organic fibers,**

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**The properties of composite linings are a function of the properties of the constituent phases (polymer matrix and reinforcing filler), their relative amounts, and the geometry of the dispersed, reinforcement**

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phase (e.g., particle size, shape, distribution, orientation). Some particulate fillers strengthen and reinforce the matrix a little, whereas others do not.

Reinforcement capability is very much size and shape dependent and elongated fibers provide the best reinforcement for plastics. The overall strength of a composite depends on the tensile strength of the fibers and on the degree to which a load can be transmitted from the matrix to the fibers. With small particle fillers having an acicular or needle-like shape (e.g., talc), a platy shape (e.g., mica), or flake shape (e.g., glass), the tensile strength is of little consequence. Small reinforcing particles restrain movement of the matrix only over a miniscule area at the particle. Tensile strength of fiber reinforcement is important and only fibers can distribute the stress over their elongated area. Only fiber-reinforced linings are well proven to have hole-bridging capability.

As with thin film linings, a white (NACE No. 1/SSPC-SP 5) or near-white (NACE No. 2/SSPC-SP 10) abrasive blast cleaning should be provided for good adhesion.

The NACE No. 10/SSPC-PA6 specification should be given consideration when designing and installing a thick-film lining system for steel bottom tanks.

#### Table 2-Thick-film, Tank Bottom Lining Resins

Glass-reinforced Lining Resins — Typical Services — Maximum Temperature Range °F (°C)

Isophthalic Polyester — Water, crude oil, distillates, and gasoline — 140–160 (60–71)

Bisphenol A Polyester — Water, crude oil, distillates, and gasoline — 160–180 (71–82)

Vinyl Ester — Water, crude oil,

aromatics, solvents, alcohols, gasohol, oil, and chemicals — 180–220 (82–104)

Epoxy (e.g., phenolics and novolacs) — Water, crude oil, aromatic distillates, and gasoline — 180 (82)

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**a. — Generally applied over a white or near-white abrasive blast cleaning in several coats. No primer is required. Information related to the performance limitations of specific coatings with regard to chemical immersion and elevated temperatures should be obtained from the lining manufacturer.**

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**b. — For tanks containing a water layer on the bottom, the maximum temperature will be at the lower end of the specified range.**

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**Installation of a chopped glass reinforced lining via a chopper gun requires applicators with specific expertise. The device held and controlled by the applicator must deposit not only the correct ratio of components in the resin mixture, but also the correct amount of fibers vs. resin. Too much resin results in a lack of reinforcement strength. Too little resin results in poor barrier properties. A reinforced lining must possess optimum barrier and stress-carrying properties.**

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**A typical installation sequence for a hand-laid mat type reinforced linings is:**

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**a. — Spray application of a resin (or flood) coat, typically 20–30 mils (635–762  $\mu\text{m}$  (m)).**

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**b. — Lay sections of pre-cut mat into the wet resin, overlapping edges of mat approx. 2 in. (5 cm).**

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**c. — Roll the resin into the mat using ribbed rollers to fully saturate it and remove entrapped air.**

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**d. — Spray apply another coat of resin, approx. 25–30 mils (635–762  $\mu\text{m}$  (m)) to achieve 45–55 mils (1143–1397  $\mu\text{m}$  (m)) total thickness.**

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**e. — Sand to remove protruding fibers.**

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**f. — Spray apply a final coat of resin (gel coat).**

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**Many types of polyester require wax addition to topcoats to ensure timely and complete surface cure. Information related to the performance limitations of specific coatings with regard to chemical immersion and elevated temperatures should be obtained from the lining manufacturer.**

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**Special consideration must be given to the coving at the transition from the tank bottom to the shell, so as to prevent cracking of the lining when the tank is put into service. As the tank is loaded, the hoop stress on the**

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shell may cause the lining to crack at the transition from the bottom to the shell if the lining is not properly supported. The manufacturer's instructions for the lining system should be followed in this regard.

### 6.3.1 Advantages of Thick-film, Reinforced Linings

Thick-film, reinforced linings are often used on aged floors that have incurred corrosion and are rough and pitted. Because they are less susceptible to mechanical damage than other linings, they would be the lining of choice for tanks in which routine personnel entry and/or mechanical work is anticipated during the life of the lining. Experience has shown that thick, glass-reinforced linings can provide sufficient strength to bridge over small perforations in the steel bottom that may develop due to soil-side corrosion. However, this benefit cannot be claimed as part of a maintenance plan because API Std 653 requires re-inspection and repair before a perforation occurs. An API Std 653 internal inspection must be performed before the steel bottom thickness is reduced to 0.050 in. (1.3 mm).

The principal advantages of thick-film, reinforced linings are as follows:

- a. Easier to achieve coverage when applied over rough, pitted steel and other surface irregularities,
- b. Ability to bridge future perforations in the floor steel,
- c. Resistant to mechanical damage,
- d. Choice of hand lay-up or chopper gun application,
- e. Few or no discontinuities to repair following the "holiday" test,
- f. Long term service greater than 20 years resulting in low life-cycle costs,
- g. Generally provides greater resistance to moisture permeation,

### 6.3.2 Limitations of Thick-film, Reinforced Linings

- a. They can require more time and effort to apply,
- b. Are normally more expensive to install than thin-film, tank bottom linings,
- c. MFL Floor Scan Inspection of the steel bottom plate through a thick-film, reinforced lining can be more difficult than a thin-film lining,

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**d. Thick film linings are more prone to cracking if tank bottom plate flexure occurs due to non-uniform soil support, and if the strain at the corner weld caused by hoop stress on the shell (e.g., filling and emptying the tank) exceeds the elastic limits of the lining.**

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### 6.34 Thick-Film, Un-reinforced Linings

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Thick-film, un-reinforced linings may be used as tank bottom linings for both new and old storage tanks. However, it is important to note that only fiber-reinforced linings are well proven to have hole-bridging capability.

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#### 6.34.1 Advantages of Thick-film Un-reinforced Linings

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a. Some thick-film linings can be built up to 100 mils (2540 μm) in a single coat.

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b. Better coverage over rough surfaces.

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c. No overlap or intercoat contamination and blushing issues with a single coat application.

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d. High solids may have better edge retention with reduced material shrinkage. Edge retention may not be an advantage on pitted floors.

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e. Typically, fast curing and can be put back in service after 24 hours at normal ambient temperatures.

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f. Few or no discontinuities to repair following the “holiday” test. This depends on the extent of pitting and application technique.

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g. Reduced labor costs compared to multi-coat thin-film or labor-intensive reinforced thick-film linings.

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h. Promotes a reduced tank turn around schedule.

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i. Long term service may be greater than 20 years resulting in low life-cycle costs.

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j. Generally provides greater resistance to moisture permeation.

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#### 6.34.2 Limitations of Thick-film, Un-reinforced Linings

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a. Typically requires the use of plural component spray equipment.

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b. Difficult to install on complex geometry due to plural component application.

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c. Contractor experience level should be a consideration.

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d. MFL Floor Scan Inspection of underlying steel condition may be limited on linings of very high thickness.

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e. Depending on resin type and thickness, cracking due to plate flexure may be a concern.

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#### Thick Film and Unreinforced

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### 6.4 Thick-Film Reinforced Linings

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There are currently two systems being specified to restore heavily corroded and pitted tank floors, Fiberglass Reinforced Plastic Laminates (FRP) and Reinforced Thick Film Linings. Fiberglass Reinforced Plastic Laminates and Reinforced Thick Film Linings each represent an important a viable alternative to replacing steel tank floors.

FRP systems consist of either an 1.5 oz glass mat or chopped fiberglass roving embedded in a resin, typically either polyester, vinyl ester or epoxy. Hand lay-up systems with glass mat do not require special equipment and can be applied with a "dump and roll method". A "chopped system" with glass roving requires heated plural spray equipment and a chopper gun to cut the glass roving and disperse it into the resin as it is being sprayed onto the floor. Chopped systems require specific applicator expertise as the device held and controlled by the applicator must deposit not only the correct ratio of components in the resin mixture, but also the correct proportion of fibers and resin.

FRP composites require multiple installation steps which include, in addition to blasting and priming, caulking of all weld seams and chine angle for smooth transition of glass, fabrication of the laminate with either glass mat or glass roving with the appropriate resin, and finally a protective gel coat of resin to insure complete wetting of the glass to prevent wicking problems.

Many tests have been performed over the years to determine the ability of FRP systems to bridge perforations due to soil side corrosion. Most published tests to date relate to FRP systems because of their 50 plus year record of successful performance. Single FRP laminates have been documented as being able to bridge perforations up to 8" in diameter with a maximum pressure of 37 psi.

Double FRP laminates have been shown to bridge perforations up to 8" in diameter with a maximum pressure of 82 psi. Since an internal hydraulic pressure of 22 psi is normal for most petroleum tanks, single or double laminates offer an added measure of protection from a leaking tank bottom.

Coating advancements developed within the past 20 years or so have produced proprietary flake and fiber reinforced thick film lining systems suitable for tank bottom restoration. These materials may be spray applied in one coat from 20.0 to 150.0 mils DFT over a blasted and primed floor that greatly reduces their installation costs relative to FRP laminates. One coat application also enhances tank turn-around time and removes inter-coat adhesion issues common with improperly installed laminates and wicking issues that have occurred with improperly wetted glass fibers. In-house testing by one manufacturer of these linings has demonstrated that a 50.0 to 60.0 mil application of their reinforced thick film lining will bridge a 2" diameter perforation under an internal head pressure of greater than 30 psi. The manufacturers typically recommend heated plural equipment for proper application which requires specialized equipment and applicator expertise.

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Any of the systems described above would be a suitable choice for tank floor restoration when poor steel conditions are found. Information related to the performance limitations of specific coatings with regard to chemical immersion, elevated exposure temperatures, and low temperature application should be obtained from the coating manufacturer. A final decision requires a determination of the current extent of topside corrosion, thickness of the tank floor, and a judgment on the potential for underside corrosion based on tank specific historical information.

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While API 653 does not allow an inspection interval whereby the steel may be expected to have perforations or be less than a minimum thickness of 0.050" with a reinforced thick film liner, the use of thick film reinforced coatings may provide a level of comfort in knowing that there is additional protection in the event that a minor perforation may occur.

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## 6.5 Circumstances Affecting Lining Selection

In addition to corrosion history and the potential for corrosion, circumstances that must be taken into account during the selection of a tank bottom lining are described in 6.5.1 through 6.5.6.

### 6.5.1 Temperature

Temperature ~~(e.g. temperature changes generated by steam coils)~~ must be taken into account during the selection of an internal lining system.

Internal steam coils, which are used to heat a product to maintain a desirable viscosity, limit accessibility to the tank bottom during surface preparation and application of the lining. As a result, a good quality installation may be difficult to achieve. In service, steam coils create local areas where the temperature can be much greater than that of the bulk product. The resulting thermal effects on a tank bottom lining may cause localized coating damage such as blistering or cracking. The distance between the coils and the tank bottom are an important factor in determining the temperatures that the coating may be exposed to. If the coils are sufficiently close to the tank floor, heat may be conducted into the floor if there is any sludge build up over the service of the tank. Storage tanks may operate above ambient temperature in order to maintain low viscosity of the stored product. As temperatures increase, this consideration becomes more critical and the need for careful lining selection is required. Information related to performance limitations with elevated service temperatures may be obtained from the lining manufacturer. ~~If this information cannot be obtained from the lining manufacturer, the owner may evaluate linings in accordance with NACE TM0174 before the selection of the lining system. Tables 1 and 2 list temperature limitations for some common generic lining systems.~~

#### Note:

The owner should always consult the manufacturer for coating selection, suitable service, temperature limitations, and curing schedule and testing procedure.

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## 6.5.2 Product Quality

With many refined products, such as gasoline, jet fuel, lubricating oils, solvents and other petrochemical products, tank bottoms may be lined not only to prevent internal corrosion but also to maintain product quality. If lining selection is principally based on product purity and the steel is in suitable condition for proper application of a thin film lining- thin-film lining systems may be suitable to fulfill this need. However, in some circumstances a combination of product quality and corrosion resistance must be considered. Coatings that are certified to MIL-PRF-23236 for fuel service must meet a range of test requirements that are designed to ensure that a lining does not negatively impact key properties of jet fuel and aviation gasoline. Coatings that are certified to MIL-PRF-4556 have tightly controlled chemical composition, which minimizes the threat of fuel contamination by the coating. MIL-PRF-4556 does not contain a test requirement to ensure fuel quality, therefore, when MIL-PRF-4556 is specified, a separate fuel degradation test such as UK Defence~~Defence~~ Note: This is the correct spelling for UK standard. Standard 80-97, Annex G may also be specified.

The owner may also have to evaluate the product immersion liquid to ensure that product contamination by the prospective internal lining will not occur. Certain products, such as fiber-grade ethylene glycol, methanol and other solvents have quality requirements that can be affected by solvent residues leaching from a newly applied lining into the stored ethylene glycol product. In the case of ethylene glycol, tThese contaminants (even at very low levels) can interfere with the quality control tests for the high purity fiber-grade ethylene glycol (used in the manufacture of polyurethane fiber). In situations such as this, linings should be evaluated to determine their suitability for the intended service. Linings intended for product quality and corrosion protection must be resistant to the intended tank service and the probable presence of a contaminated water layer on the floor. The manufacturer shall be advised of the type of testing for product contamination that the lining will be subjected to in order to determine if the lining selection is suitable for the service.

### 6.5.3

### 6.5.3 Presence of Tank Internals

Existing tanks may have design and fabrication features that make the application of a lining impractical or can seriously jeopardize the integrity of a lining. Examples of this include the coil supports and striker plates and cone roof legs. The detail for the termination of the coatings where these features are encountered are critical to a good installation. For example, steel reinforcing or striker plates should be fully welded to the tank floor where feasible. Floor coatings can properly be terminated on these reinforcing plates. The owner can select to coat or not coat items such as cone roof columns and coil supports that are designed to be free from connection with the floor or are designed to be self-centering. When electing to terminate a coating on a bottom reinforcing plate near a feature, it is important that the surface preparation be performed to the specification

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beyond the location of the coating termination. The coating should be terminated in the reinforcing plate no less than 2 inches from any weld if feasible. If it is suggested to coat the striker plates, the coating should be performed before the plates are installed, leaving the weld areas for field coating installation. For example, internal steam coils, which are used to heat a product to maintain a desirable viscosity, limit accessibility to the tank bottom during surface preparation and application of the lining. As a result, a good quality installation may be difficult to achieve. In service, steam coils create local areas where the temperature can be much greater than that of the bulk product. The resulting thermal effects on a tank bottom lining may cause localized coating damage such as blistering or cracking.

#### **6.5.4 Flexibility for Service Change**

Changes in tank service may affect the performance of an existing tank bottom lining. Tank linings do not offer universal resistance. A properly applied tank bottom lining may provide more than 20 years of service life in storing a particular product. A lining that has provided many years of satisfactory protection in one product may have inadequate resistance to a new service environment. The need for operational flexibility at some facilities requires that some tanks be available for swing service. Such factors should be considered during the selection and design of a lining system. Many linings will need to recover between product changes. Consult the manufacturer to determine if there are any specific recommendations when changing product stored.

#### **6.5.5 Construction Details that Can Impact the Lining**

It is difficult to achieve lining continuity when irregular surfaces caused by discontinuous connections such as rivets, butt straps, and skip welding exist because they are difficult to cover and protect with a lining. In old tanks, the problem of poor coverage may be complicated by chemical contaminants, which may be difficult to remove. It is common to use caulk to seal lap joints between riveted plates and around rivets to provide a continuous surface for the lining application. Caulking shall be selected and specified based on the conditions encountered with consideration for the temperatures and the tank service requirements. Welded tanks generally require less preparation than riveted tanks. See NACE 10/SSPC-PA6 Fiberglass-Reinforced Plastic (FRP) Linings Applied to Bottoms of Carbon Steel Aboveground Storage Tanks for information on caulking.

Note that caulk may be used with thin film lining systems as well as ~~unreinforced-thick film linings~~ where needed to work with surface irregularities.

Consideration should be given to the design of the striker plates beneath the cone roof support columns and internal floating roof legs. Abrasion may occur from contact between the legs and the tank floor. While coatings may be required on the tank floor, a steel striker plate that is fully seal welded will act as protection of the tank bottom. Coatings may or may not have to be continuous beneath the legs, depending on the details concerning the installation of striker plates. If striker plates are not installed, a provision must be made (e.g. protective teflon shoes or similar) to protect the coating in the event that the roof lands. Cable suspended roofs have made this detail moot. ~~mm~~ systems where needed to work with surface irregularities.

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~~Support steel under cone roof column supports or floating roof support column landing plates may be necessary to protect the floor and the lining from impact and wear. Note: This deserves its own section above.~~

~~The type and extent of previous repairs to the tank (such as internal lap patches or nozzle additions with no back weld) should be taken into consideration. How?~~

## 6.5.6 Upset Conditions

The degradation of a lining is a complex process and, unlike the steel that is to be protected, degradation is not readily quantified by a corrosion rate. A relatively short-term exposure to an unusually aggressive environment can cause irreversible damage to a lining, compromising the protection afforded to the steel. For this reason, a lining must resist potential upset conditions in addition to the usual service environment.

## 7 Surface Preparation

### 7.1 General

As recommended in the scope of this document, NACE No. 10/SSPC-PA 6 and NACE No. 11/SSPC-PA 8 should be considered when determining specific criteria for surface preparation and lining application. Following is a general outline of surface preparation considerations covered in these referenced documents.

Surface preparation is a critical part of the lining application. Continuous immersion is a severe exposure. Inadequate surface preparation is a major cause of lining failure. Surface preparation is performed to provide the appropriate combination of surface cleanliness and surface profile, or the anchor pattern (see 7.5) required to establish good chemical and mechanical adhesion of the lining resin to the steel. Generally, abrasive blast cleaning to a white metal finish (NACE No. 1/SSPC-SP5) is desired. Abrasive blast cleaning to a near-white metal finish (NACE No. 2/SSPC-SP10) is often specified as the minimum degree of surface cleanliness. For small areas, SSPC SP 11 is often desirable to avoid damage to the surrounding lining that may be in very good condition. Use of power tools to meet SSPC SP 11 requirements must include the use of abrasive disks or flapper wheels that provide the specified anchor profile and must be followed by solvent wipe per SSPC SP 1 to remove oil contaminants from the power tool.

To facilitate inspection and to ensure good adhesion of the lining, surface preparation by abrasive blasting should extend several inches beyond the area to be lined. This practice of framing the area where lining is to be applied helps to ensure that unprepared steel is not inadvertently coated.

### 7.2 Pre-cleaning

#### 7.2.1 Residue Removal

Prior to abrasive blasting, all hydrocarbon residues such as oil, tar, and grease, must be removed from the area to be lined. Solvent cleaning (see SSPC-SP 1) and high or ultra-high pressure water or steam cleaning, using the proper chemicals, are effective methods of accomplishing complete hydrocarbon removal. Cleaning is typically followed by a fresh water rinse to ensure complete removal of cleaning chemicals.

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### 7.2.2 Soluble Salts

It is important to note that typically abrasive blasting is not effective in the removal of soluble salts. The presence of soluble salts on the steel can adversely affect the performance of a lining resulting in blistering by osmosis. Consideration should be given to a field evaluation for the presence of soluble salts whenever there is the possibility of such contamination. [SSPC-TU-4 Guide 15](#) describes common methods for this evaluation. The use of high pressure and ultra-high pressure water jetting NACE No. 5/SSPC-SP 12 ~~can reduce~~ ~~has proven to be effective in the reduction of~~ soluble salt ~~contamination, contamination; however an acceptable reduction may not occur due to the presence of chemically adsorbed molecules.~~ Typically ~~the NACE No. 5/SSPC-SP 12;~~ this specification is used for substrates that already possess a surface profile and do not require abrasive blasting.

~~Commercial products assist in reducing the presence of soluble salts if they are found on the substrate during testing. Follow the manufacturer's recommended procedures for use of these products. Be sure to test again following any treatment method. For substrates that require a surface profile, there are commercial products available that can be added to a water wash to reduce the presence of soluble salts prior to abrasive blasting.~~

### 7.2.3 Water Quality

~~Water that is used for surface cleaning should be of sufficient purity and quality that it does not preclude the surface from meeting the surface cleanliness criteria. Where salt water is used for hydrostatic testing, the substrate should be tested for contaminants prior to the start of the lining process. Different cleaning and treatment may be required to return the substrate to acceptable condition~~

## 7.3 Bottom Repair and Weld Preparation

The ~~preferred~~ only technique for the repair of perforations of the steel tank bottom is welding of steel patches. ~~Epoxies shall not be used to repair perforations.~~ API STD ~~653~~ 653 should be consulted for information on tank bottom repair.

Welds should be inspected before and after blast cleaning. All sharp edges and protrusions should be ground to provide a smooth surface that can be completely and uniformly covered with the lining material. Sharp edges and protrusions may be caused by such things as weld spatter, sharp weld crests, undercutting of the weld, arc burns, erection clips, plate joints, burrs, and gouges. Chipping, followed by grinding, can be used to remove sharp edges. NACE RP0178 can be used to specify the surface finish of welds. Typically, weld finish "C" or "D" is specified where feasible.

## 7.4 Surface Cleanliness Environmental Conditions During Blasting

~~Abrasive blasting should not be performed if the temperature of the steel surface is less than 5°F (3°C) above the dew point or if the relative humidity is greater than 80% (see 8.3).~~

~~Note this item on dew point and humidity is repeated below in 8.3~~

The surface to be lined should be of the specified level of cleanliness at the time the lining is applied. If the surface is degraded or contaminated subsequent to surface

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preparation and before lining application, the specified level of cleanliness should be restored before lining application. Holding primers must be applied before the surface has degraded if specified. It may be difficult when using recycled media on tank linings to ensure that the surface is clean. Recycled media may collect contaminants on each successive recycle process and impinge these contaminants into the steel profile which are often difficult to detect by inspection. Owners should weigh the benefits of recycled media against the risk of having surface contamination that may interfere with the life of the internal lining.

### 7.5 Surface Profile or Anchor Pattern

The abrasive used for blasting should be selected to produce the necessary profile depth, or anchor pattern, for the lining to be applied. The lining manufacturer's recommendation for surface profile depth must be achieved in order to optimize the mechanical adhesion of the lining to the steel tank bottom. The anchor pattern required for linings is typically 1.5 – 4.0 mils (38 – 102 ~~microns~~<sup>µm</sup>) and generally increases with the thickness of the lining. To achieve adhesion necessary for long-term performance, it is important that the anchor pattern is sharp and angular. It may be difficult when using recycled media on tank linings to ensure a uniform proper profile depth as well as a proper degree of sharpness and angularity. Owners should weigh the benefits of recycled media against the risk of not having adequate surface profile that may be required for internal linings.

### 7.6 Air and Abrasive Cleanliness

The abrasive and compressed air supply used for abrasive cleaning of tank bottoms should be free of contaminants such as water soluble salts, dirt, clay, oil, and grease (per SSPC AB1, AB2, AB3, and ASTM D 4940, as appropriate). If present in the blasting abrasive, small amounts of these contaminants may be delivered to the steel surface during the cleaning operation. This contamination will reduce the useful life of the lining.

### 7.7 Removal of Salts

Corrosion inducing anions from water soluble salts, if present, may be lodged on the substrate surface. Section 7.2.2 covers soluble salts and their treatment. Testing for the presence of chloride and other contamination should be considered prior to proceeding with any lining installation. **7.7 Removal of Salts**

~~Corrosion inducing anions from water soluble salts, if present, will be lodged on the substrate surface below the mill scale and insoluble rust products formed over the steel surface. Testing of the surface immediately after high pressure water washing or abrasive blasting will determine their presence. There are commercial products which can be added to a water wash to reduce the presence of salts. Assessment of their specific effectiveness can be determined on test surface areas or by confirmation of accepted impartial data. The coating manufacturer can provide information on the compatibility of the salt remover with the coating to be applied.~~

~~This section is a duplication of 7.2.2. It should be combined with 7.2.2 and eliminated. It belongs in pre-cleaning section.~~

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## 7.7.8 Removal of Dust

Spent abrasive ~~-as well as spent abrasive (dust)~~ must be removed from surfaces prior to coating application. Standard practice has been to blow-down surfaces with clean, compressed air, and use vacuum cleaning methods. Follow OSHA regulations when considering use of compressed air for cleaning surfaces. but this can be a messy operation, especially in small tanks. Vacuum cleaning methods have proved to be more efficient. ISO 8502-3 may be used to determine the effectiveness of cleaning methods.

## 8 Lining Application

### 8.1 General

~~For thick film laminates, the coating manufacturer may recommend that a prime coat be applied at a film thickness less than that of the anchor pattern achieved by the abrasive blast cleaning. If a primer coat is applied, it is important to follow such instructions to prevent disbonding or delamination of the subsequently applied lining. Experience has shown that it is difficult to consistently apply primer coats at the low thickness required. When not mandatory, it may be better to omit the primer. When a holding primer is used, it is important that it is applied according to the manufacturer's instructions for film thickness as excess thickness may have an adverse affectadverse effect on intercoat adhesion and will adversely affect the negative influence on performance of the coating system. Recoat windows must be strictly followed when using multi coat systems. If coatings exceed the suggested recoat windows, then the coating must be properly prepared in accordance with the manufacturers recommendations prior to proceeding to any subsequent coats or processes.~~

Subsequent coats must be applied within the recoat interval recommended by the lining manufacturer ~~and/or as determined by the owner's inspector. Note: This determination is beyond the scope of the inspector. The inspector shall follow the specifications and the manufacturer's specifications for the product as well as the complete coating system. The inspector shall record and report to the owner the conditions and the time intervals.~~

Generally, the recommendations and procedures prescribed in SSPC-PA 1 should be followed. After sufficient curing of the completed lining, holiday testing (as described in 9.3.4) should be carried out. Any defects should be repaired in accordance with the coating material manufacturer's recommendations and the written specification.

### 8.2 Guidelines for Lining Application

SSPC-PA 1 provides general guidelines for good lining application practice. Proper on-site storage conditions, mixing, applying, and curing of the lining are essential procedures, and the lining manufacturer's recommendations should be followed. Any differences between the owner's specification and the lining manufacturer's recommendations should be resolved before beginning the job.

### 8.3 Temperature and Humidity Control

The temperature of the steel surface should conform to the lining manufacturer's recommended application and curing ranges. As a general rule, the surface temperature must be at least 5°F (3°C) above the dew point temperature in the tank and the relative

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humidity should be below 80% at the steel surface. If the surface temperatures and/or humidity level expected to deviate from the recommended range, ~~temporary~~ climate control equipment should be employed to ensure the proper conditions are maintained. It should be noted that durations of surface preparation, lining application, and cure may be continuous over a 24-hour period. If so, the required environmental conditions must be maintained around the clock. Owner operations may interfere with continuous use of environmental control equipment. These operational considerations should be reviewed prior to the execution of the tank lining project.

NACE 6A192/SSPC-TR 3 provides guidance on the use of dehumidification and heating equipment for environmental controls during tank lining work.

~~Temporary~~ climate-control equipment is also used to advantage by protecting workers from heat stress during hot summer months. Improved productivity, due to better working conditions, is a secondary benefit.

#### 8.4 Lining Thickness

Insufficient film thickness will not provide adequate coverage or protection and can result in reduced service life of the lining. Excessive film thickness beyond the manufacturer's recommended range can compromise lining adhesion and film integrity. ~~Excess primer thickness is a common cause of failure of thick film lining systems. Note: This is a repeat from section 8.1 Excess primer thickness is a common cause of failure of thick film lining systems.~~ The lining thickness shall be in accordance with the lining specification. Excess thickness of any particular coat shall be remedied in accordance with the manufacturer's recommendations prior to proceeding to any subsequent coats or processes. Thickness should be determined in accordance with the methods outlined in 9.3.2. Changing or alternating colors between coats can aid in assuring uniform coverage and thickness.

#### 8.5 Lining Curing

Improper application and inadequate curing time are major causes of premature lining failure. The adhesion and integrity of the film are adversely affected if a lining has not been applied and cured properly. Prior to removing forced ventilation or closing the tank, the lining should be completely cured to obtain optimum service life. Refer to the coating manufacturer to determine the proper cure time and temperature. The proper curing conditions should be ensured for the full duration of the cure time where feasible. ~~Those proper conditions or~~ forced-curing of the lining may be accomplished by circulating warmed, dehumidified air (see 8.3 and NACE No. 10/SSPC-PA 6).

The owner shall not rely on estimates of time and ~~temperature~~ temperature. The owner and the applicator shall ensure that the lining is fully cured for service by any of the methods specified to determine complete cure prior to returning the tank to service.

Solvent-borne linings require forced ventilation of the air space adjacent the lining. As the heavier-than-air solvents evolve from the wet lining, they will rest atop the lining, impairing the completion of this process. Dissipation of solvent vapors must occur so enough solvent can evolve from the film to achieve a level of cure necessary for hydrocarbon or chemical resistance.

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## 9 Quality Control Inspection

### 9.1 General

~~Independent Quality Assurance inspection is highly recommended to oversee the Contractor's quality control process. This shall and strict adherence to the manufacturer's requirements is strongly recommended to ensure that the criteria in the lining specification have been met. The lining should be inspected during all phases of the work and upon completion of the work. The performance life of a lining is directly related to the quality of the surface preparation, application and curing, combined with thorough inspection and complete documentation throughout the entire process. Documentation~~ Documentation should include daily inspection records to capture the project activity and issues per the written specifications.

~~Project R~~ Records should be made to briefly describe the products and procedures that were used during installation of the lining. ~~These R~~ Records will be important the next time the tank is opened to associate the lining product and installation process with the lining performance. Records will also be valuable if repairs are needed and a repair product and repair procedure must be developed.

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### 9.2 Qualification of Inspection Personnel

All lining inspectors should be either NACE or SSPC certified, or ~~should persons who~~ have demonstrated a thorough knowledge of coating and lining practices.

### 9.3 Recommended Inspection Parameters

#### 9.3.1 Surface Cleanliness and Profile

~~Quality assurance and quality control personnel shall verify that the recommended practices reviewed in Section 7 as well as the manufacturer's specifications are strictly followed. In the case of a conflict the manufacturer's specifications shall govern.~~

~~Verification that the specified surface cleanliness and profile have been achieved before application of any lining is of utmost importance. It is important that the coating be completed before any flash rusting is observed. SSPC VIS 1 provides reference photographs that may be used to visually assess surface cleanliness. In addition, ISO 8502-3 provides an assessment of dust on steel surfaces prior to the application of the lining. Surfaces should be tested for the presence of invisible corrosion inducing salt anions on the surface prior to lining due to the well established effect the salts have on life cycle performance. SSPC Guide 15 offers information of commercially available surface testing methods. NACE RP0287 provides a method of measuring surface profile. Other types of profile comparators are available from the SSPC and coating instrument vendors.~~

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#### 9.3.2 Film Thickness

~~Inspection shall verify that a-~~ As the lining is being applied, wet film thickness measurements should be made in accordance with ASTM D 4414. After the lining has cured sufficiently to allow handling, dry film thickness measurements should be made in

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accordance with the specified method to determine dry film thickness or -SSPC PA 2, if not otherwise stated.-

### **9.3.3 Final Cure Hardness**

If specified to aid in determination of degree of cure, hardness of the lining should be measured in accordance with manufacturer's recommendations following any specified ASTM methods D 2583. It should be noted that this test could be destructive to organic resin linings that are not sufficiently thick, hard, and/or cured.

### **9.3.4 Lining Discontinuities**

Holiday testing of thick-film linings shall be carried out with a high-voltage detector in accordance with NACE RP0188. Holiday testing of thin-film linings should be performed with a low-voltage (67.5 volts) wet sponge detector. When testing with high voltage detectors it is important that the voltage be properly set in accordance with the manufacturers recommended volts per mil and that the film thickness properly matches the specified thickness. Otherwise, damage may occur from the testing operation. Also, nothing in this document shall preclude the testing of a thin film lining using a high voltage detector, if there are temperature considerations, provided that the voltage be properly set to correspond with the film thickness.

## **10 Evaluation and Repair of Existing Linings**

### **10.1 General**

A properly selected and applied tank bottom lining should be expected to provide a minimum service life of 20 years. Some lining systems, most notably thick-film laminates, have provided 25 – 30 years of service life. Lining “failure” is not well defined and fitness for service is not well established for polymeric coatings. Linings degrade with time. However, blistering is a common mode of lining deterioration. However, blistered linings may remain fully functional, providing corrosion protection to the steel for many years. Lining degradation does not necessarily translate to putting the steel at significant corrosion risk.

When available, tank bottom linings should be thoroughly inspected to assess their condition and determine the need for any repairs. Timely maintenance can keep repairs to a minimum and greatly extend lining service life. Care should be taken not to damage the lining (especially thin-films) during cleaning, and inspection and mechanical repair procedures. API STD ~~653~~ provides guidance for visual in-service and detailed out-of-service inspection and repair methods for tank components. These inspections may reveal conditions that necessitate lining repair, which are not covered in API S ~~TD~~ 653. All repairs to the tank should be completed before any repair of the lining.

### **10.2 Evaluation Methods**

Lining evaluation methods include:

- a. Visual inspection.
- b. Adhesion measurement.

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- c. Audible testing (to find areas of delamination on thick film reinforced linings via tapping with a solid metal object).
- d. Physical examination of lining sample, including possible laboratory testing (to determine permeation by the tank's previous product, film thickness, brittleness, and/or adequacy of cure).
- e. Holiday testing (This is not typically recommended for linings that have been in previous service, since the presence of moisture in the film can cause damage when exposed to voltage. In some instances, this has been successfully achieved after tank has remained open and the lining exposed to normal ventilation for several months. Consultation with the coating manufacturer prior to attempting this type of inspection is necessary).

Note: This holiday test requirement may propose a challenge as many regulatory agencies rely on the holiday test to establish the efficacy of a lining that has been in service. If a lining that has been in service fails the holiday test in areas that are not obviously deficient, the holiday test should not be used as the only criteria. Visual inspection and professional judgment are required to determine the extent and feasibility of repairs to the existing lining along with judgment with respect to the remaining service life of the lining for purposes of API 653 requirements. Adequate cleaning of the tank is critical to successful and meaningful holiday testing of tank linings that have been in service.

### 10.3 Evaluation Criteria for Linings

Evaluation of existing tank linings should be based on the following criteria:

- a. How long has the existing lining been in-service?
- b. How well has the existing lining performed to date?
- c. The desired service life of the lining (i.e. how long must the lining do its job before it will be inspected and receive required maintenance?)
- d. The intended exposure conditions (i.e. intended service of the tank, operating temperature, whether water will be present, whether other contaminants or chemicals will be present and their concentrations).
- e. The specifications and characteristics of the existing lining.

### 10.4 Evaluating Serviceability of Existing Linings

The evaluation methods listed in 10.2 should be used to determine if an existing lining is suitable for service. Blistering, cracking, crazing, discoloration, and areas of missing lining are modes of degradation that can be detected by visual inspection. However, these types of degradation may not be readily visible unless the floor is thoroughly lighted, cleaned, and accessible. Other modes of degradation, that may not be readily visible, are permeation of the lining by hydrocarbon, delamination, and loss of thickness due to abrasion and/or chemical attack. These modes of degradation may require the use of the other examination techniques in 10.2 to be detected. Following the examinations, the evaluator should apply the criteria in 10.3 to determine if the lining is suitable for service.

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## 10.5 Determining the Cause of Lining Degradation/Failure

If lining degradation is detected, the cause and extent of coating degradation must be established, as well as whether or not the existing lining is suitable for a repair. When evaluating the condition of an existing lining, one should consider whether deterioration is premature or whether the lining has achieved its anticipated performance life.

If degradation or failure of a lining is premature, it is important to understand and address the cause of such degradation prior to determining whether the lining should be allowed to be repaired, ~~or~~ refurbished ~~or should vs. be~~ completely replaced. A review of the tank's operating history and a visual examination of the lining should be conducted to determine whether the problems were a result of environmental attack, local mechanical damage, and/or if inadequate surface preparation or improper lining installation were contributing factors.

## 10.6 Lining Repair and Replacement

The term "repair" of a lining is typically used when either portions of the lining will be replaced or when all or a portion of the lining will be ~~topcoated~~ top coated. The term "replacement" is used when all of the existing lining is completely removed to the steel substrate and a new lining is applied.

### 10.6.1 Lining Repairs

#### 10.6.1.1. Localized vs. General Degradation

The amount of the floor area that has failed or deteriorated and the size of the tank are significant factors in determining whether only portions of, or the entire lining, should be replaced. If only a few, small areas require lining replacement, and the tank is fairly large, it is usually more cost effective to use power tools to achieve the required level of cleanliness and anchor profile depth rather than to introduce abrasive into the tank. For thin-film linings in good condition, open blasting in a tank is not advised as the removal of the abrasive material often damages the existing lining. When new patch plates are installed as a result of an API 653 inspection, it is important that the patch plates be properly cleaned and properly profiled in accordance with the lining manufacturer's requirements for immersion service. This is especially true if power tool cleaning is used in lieu of abrasive blast cleaning on the new plates.

#### 10.6.1.2 Spot Repairs

Spot repairs are made when there are only localized failures, such as blisters, pinholes, delamination, or mechanical damage. Usually, the existing lining is removed, the surface is prepared, and lining materials are applied at the failed areas only.

#### 10.6.1.3 ~~Topcoating~~ Top coating an Existing Lining

Thick-film reinforced linings can be ~~topcoated~~ top coated to extend the life of an existing coating that has good adhesion and integrity. The topcoat is applied to ensure the fibers are not exposed to the product. Accepted practice involves removal of contaminants, then brush-blasting and application of one or more topcoats. To ensure good adhesion of the

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repair, the lining manufacturer should be consulted to assess the compatibility of the topcoat material with the existing lining. Thin film and thick film reinforced and unreinforced linings may be topcoated as part of a repair procedure in certain situations depending on the condition of the existing coating and the extent of holidays and coating repairs required.

#### **10.6.1.4 Repair or ~~Topcoating~~Top coating Specifications**

Consideration should be given to the lining manufacturer's recommendations when developing the repair specifications. All differences between this recommended practice and any other should be resolved before starting any lining repairs.

#### **10.6.1.5 Lining Removal Methods**

Considerations that affect the method of lining removal are:

- a. Size of repair.
- b. Type of lining.
- c. Whether steel is contaminated with oil or chemicals.

If the mode of degradation of a thick-film, reinforced lining included delamination, it should be noted that manual removal of the un-adhered laminate is more cost effective.

Care must be taken with manual and power tool removal of linings to avoid damage to the floor and lower shell substrate from gouging. Techniques such as electromagnetic induction and ultra-high water blasting may be more effective in removing failed laminates and should be considered as an alternative to power tool cleaning or abrasive blasting.

#### **10.6.1.6 Sequence of Contamination Removal vs. Lining Removal by Blasting**

Regardless of whether a lining will be completely removed and replaced or will receive spot repairs or ~~topcoating~~top coating, it is important to detect and to identify visible and/or non-visible contaminants. If such contaminants include hydrocarbons, grit blasting without first removing the oily hydrocarbon may adversely affect the new lining's adhesion. If oily hydrocarbon has come into contact with the steel, it is critical that the contaminant be removed before abrasive blasting.

### **11 Maximizing Lining Service Life by Proper Material Selection and Specification**

API Std 653 specifies the maximum interval between internal tank inspections to be 20 years without the application of alternate internal inspection intervals determined by risk-based inspection. Corrosion on the topside of the tank bottom is a factor in determining a proper interval between tank inspections. Corrosion protection afforded by an internal lining mitigates the corrosion rate on the topside of the tank bottom and allows the service interval between tank inspections to be maximized.

However, linings do not last forever. Typically, they become less effective over time. The deterioration rate can be fast or slow. Experience has shown that some linings have failed

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in less than a year and some linings have been found to provide adequate corrosion protection after more than 20 years of service.

~~Keith to work transition wording between the above and Section 11.0~~

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## 11.1 Lining Material Selection

Unless the specifier has experience with a given lining material's performance in a given service, ~~the owner/operator should require verifiable test data along with the owner/operator he/she should require third party verifiable test data along with and~~ references supporting the considered material's suitability for the intended service and operating conditions.

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## 11.2 Written Specification

The specification should be very job-specific and include a detailed scope, a specific description of the components to be lined, and a list of all responsibilities and tasks of the contractor. As a minimum, the specification should address the relevant aspects covered by NACE No.10/SSPC-PA 6 and NACE No. 11/SSPC-PA 8 as follows:

- a. Steel plate preparation and weld surface quality.
- b. Applicator qualifications and submissions.
- c. Surface preparation, including criteria describing the abrasive, steel cleanliness, anchor profile, removal of dust, ~~salts and other~~ contaminants, ~~and~~ waste handling, and removal.
- d. Environmental controls.
- e. Control of solvent vapors.
- f. Need for wet film thickness measurements.
- g. Applicable heat curing requirements.
- h. Dry film thickness range required and criteria as to method of measurement.
- i. Holiday testing requirements.
- j. Method for determination of cure.
- k. Final inspection requirements.
- l. Labeling or stenciling requirements for lining identification.
- m. Inspection requirements.

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## 12 Health, Safety and Environmental

### 12.1 General

Prior to the application of internal tank linings, proper training of employees regarding ~~health, safety safe work and environmental~~ procedures and the provision of the necessary supervision and/or inspection throughout the progress of the job is required. Guidance on federal training requirements is given in OSHA 2254. A documented hazard evaluation

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as outlined in OSHA 29 CFR 1910.132 is required to determine what personal protective equipment (PPE) may be needed.

~~This section will not attempt to detail all of the safety precautions and procedures required to safely enter a tank, prepare the necessary surfaces for lining, and apply the specified lining material. Some of this information is presented in regulatory and industry documents. General safety concerns are emphasized in 12.2 through 12.4.~~

~~Users of this recommended practice are responsible for reviewing appropriate health, safety, environmental and regulatory documents and for determining their applicability in relation to this recommended practice standard prior to its use. This recommended practice does not address all potential health and safety issues or environmental hazards associated with the use of materials, equipment, and/or operations detailed or referred to within this recommended practice. Users of this recommended practice are also responsible for establishing appropriate health, safety and environmental protection practices, in consultation with appropriate regulatory authorities if necessary, to achieve compliance with any existing applicable regulatory requirements prior to the use of this recommended practice.~~

~~General health and safety concerns are emphasized in 12.2 through 12.4.~~

## 12.2 Tank Entry

All necessary precautions to protect personnel shall be taken before entry and while working in a storage tank. Working in a confined space such as a petroleum storage tank presents special respiratory, explosion, and fire hazards that must be addressed. Tank entry and/or hot work permits should be issued and enforced as local work rules and applicable regulations require. Guidelines for issuing permits and preparing a tank or confined space for entry are detailed in API STD# 2015 and RP 2016, including evaluation of the atmospheric hazards and lockout-tagout of process lines and equipment. Federal, ~~s~~(OSHA 29 CFR 1910.146) and ~~s~~State, ~~or where applicable, International and local~~ regulations (or international regulations if applicable) pertaining to confined space entry also should be reviewed and followed to ensure conformance. ~~In the US, (OSHA 29 CFR 1910.146 governs permit-required confined spaces under the OSHA General Industry standard.)~~

## 12.3 Surface Preparation and Lining Application

Health hazards are a prime concern during surface preparation and lining application. Proper respiratory equipment and personal protective clothing should be employed where necessary. Information regarding safety precautions and procedures during surface preparation and lining application are found in ~~OSHA 29 CFR 1910.94, and~~SSPC PA 3.

Note: This is the general industry standard for ventilation and abrasive blasting and really covers shop operations. Most of the provisions do not really apply in the field conditions. There is no abrasive blasting standard under Construction Standards.

If lining materials containing or previously exposed to lead are to be removed, special precautions are required to protect both the personnel and the environment. The specific requirements for worker protection from lead can be found in OSHA 29 CFR 1926.62f.

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~~Construction Industry Standard is more stringent and applies to most tank repair work. Relevant federal and state regulations should also be reviewed to ensure conformance.~~

#### 12.4 Manufacturer's Material Safety Data Sheets

The chemical ~~constituents~~~~make-up~~ of high performance, internal tank lining materials can present health hazards to workers if not handled properly. Material safety data sheets (MSDS) concisely inform employees about the materials being used so that they can protect themselves and respond properly to emergencies.

The purpose of an MSDS is to ~~inform~~~~teH~~ the worker:

- a. A material's physical properties, which make it hazardous to handle.
- b. The type of personal protective equipment needed.
- c. The first aid treatment necessary if exposed to a hazard.
- d. The planning needed for safely handling normal operations, as well as emergencies such as spills and fires.
- e. The appropriate response to accidents.

The applicable MSDS should be consulted for all materials before conducting any work.

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